ANTENNA CHARACTERISTICS OF HETERODYNE RECEIVERS OF CO2 LASER EMITTERS

I.I. Dushkov, N.V. Karlov, B.B. Krynetskiy, V.A. Mishin and R.P. Petrov

(NASA-TT-F-15968) ANTENNA CHARACTERISTICS OF HETERODYNE RECEIVERS OF CO2 LASER EMITTERS (Kanner (Leo) Associates) 8 p HC \$4.00 CSCL 20E

N74-34014

Unclas G3/16 50393

Translation of "Antennyye kharakteristiki geterodynnogo priyemnika izlucheniya CO2-lazerov," Kratikiye Soobshcheniya po Fizike FIAN, No. 1, 1971, pp. 40-44



			31 AN	DARD THE PAGE
1. Report No. NASA TT F-15,968	2. Government Ac	ccession No.	3. Recipient's Cata	log No.
4. Title and Subtitle	-	5. Report Date		
ANTENNA CHARACTERISTICS OF HETERODYNE			October 1974	
RECEIVERS OF CO ₂ LASER EMITTERS			6. Performing Organization Code	
7. Author(s) I.I. Dushkov, N.V. Karlov, B.B. Krynet-skiy, V.A. Mishin and R.P. Petrov			8. Performing Organization Report No.	
			10. Wark Unit No.	
			11. Contract or Grant No.	
9. Performing Organization Name and Address			NASw-2481	
Leo Kanner Associates Redwood City, California 94063			13. Type of Report and Period Covered Translation	
National Aeronautics and Space Adminis- tration, Washington, D.C. 20546			14. Sponsoring Agency Code	
15. Supplementary Notes				
Translation of "Antennyye kharakteristiki geterodynnogo priyemnika izlucheniya CO2-lazerov," Kratikiye Soobshcheniya po Fizike FIAN, No. 1, 1971, pp. 40-44				
16. Abstract				
An experimental setup for measurement of antenna characteristics of a heterodyne receiver of CO ₂ laser emitters and its operation are described and illustrated. A 6.6 W LG-17 CO ₂ laser, with a 0.005 rad divergence, was the radiation source, the Doppler frequency shift device provided a frequency shift of 20 MHz, and Ge-Au and Ge-Zn-Sb photoresistors, with 2 × 2 mm detection area, at a temperature of 78°K, was used. A 20 dB gain and a 15-fold narrowing of the directivity pattern, to 0.007 rad, were achieved. Comparison of the experimental curves presented shows that generalized reciprocity theorem can be used to estimate the directivity of a heterodyne detector. It is stated that use of a nonlinear element can eliminate the possibility of failure to detect a weak signal due to atmospheric turbulence.				
17. Key Words (Selected by Author(s))		18. Distribution Statement		
		Unclassified-Unlimited		
19. Security Classif. (of this report)	20. Security Class	sif, (of this page)	21. No. of Pages	22. Price
Unclassified	Unclassified		6	1100

ANTENNA CHARACTERISTICS OF HETERODYNE RECEIVERS OF CO2 LASER EMITTERS

I.I. Dushkov, N.V. Karlov, B.B. Krynetskiy, V.A. Mishin and R.P. Petrov

The directivity of a heterodyne receiver of CO_2 laser $\frac{40}{*}$ emitters was investigated directly, and by means of the generalized theorem of reciprocity. It was found that, with a heterodyne detector for a receiver, with a sensitive area of 2 × 2 mm², the directivity pattern is narrowed to 0.007 rad.

Coherent detection was carried out earlier in the visible and IR ranges [1, 2]. There is particular interest in heterodyne detection of $\rm CO_2$ laser radiation, which is explained by the high power of $\rm CO_2$ lasers, as well as by the 8-14 μ transparency window in the atmosphere. Heterodyne detection sharply attenuates the effect of various noise sources, including the effect of black body radiation, existing at the 10.6 μ wavelength, at a temperature of 300°K. An increase in ν 1) selectivity is accompanied by an increase in k selectivity, since heterodyning is subject only to those types of signal fluctuations, which are excited in the body of the detector by heterodyne radiation, to which attention was first drawn, in connection with the problem of sensitivity, in [3].

Analysis [4] has shown that, by matching the heterodyne field and the signal in the plane of an optical detector, the intermediate frequency signal is proportional to the ratio $[\sin(\pi d\alpha/\lambda)]/(\pi d\alpha/\lambda)$, where α is the slope angle of the signal front relative to the heterodyne front, d is the diameter of the signal beam cross section and λ is the light wavelength. From the point of view of antenna theory, this is equivalent to the

/41

^{*} Numbers in the margin indicate pagination in the foreign text.

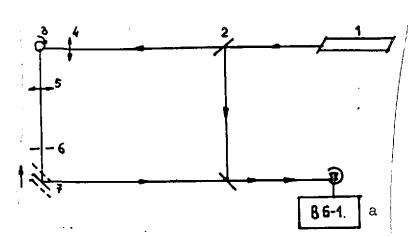


Fig. 1. Key: a. V6-1

assertion [5] that an optical heterodyne detector is characterized by an effective area S_n , connected with the solid detection angle Ω , by a limitation of the type $S_n\Omega_n \stackrel{\sim}{\sim} \lambda^2$. In this case, the optical elements located in the paths of the signal and heterodyne beams (or in the path of one

of them) can change the ratio of S_n and Ω_n , but cannot change the value of their product.

In our experiment, measurement of the antenna characteristics was carried out according to the following scheme (Fig. 1): radiation from the CO₂ laser (1), passing through beam-splitting mirror (2) (the branched power was used as the heterodyne signal), was focused on a device, creating a Doppler shift of the signal frequency (3). The signal fell on scanning mirror (7) through converging lens (5) and diaphragm (6). The signal reflected from the scanning mirror was added to the heterodyne signal in second beam-splitting mirror (8), after which both signals fell on the photosensitive surface of photoresistor (9). Displacement of the scanning mirror changed the angle of incidence of the signal beam and made it possible to measure the detector directivity pattern. The frequency difference signal was recorded.

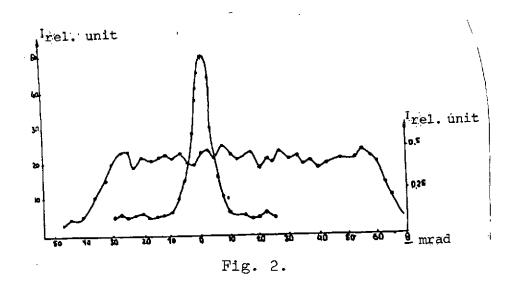
<u>/42</u>

A standard CO₂ laser (LG-17), with a 6.6 W output power and 0.005 rad divergence, was used in the experiments. The laser operated in the ${\rm TEM}_{\rm Olq}$ mode. The beam splitter was made of ${\rm BaF}_2$.

The signal frequency Doppler shift device was a six-pointed star, 20 mm on a side, fastened to the axle of a DID-2 motor. At a rotation frequency of 330 Hz, the frequency shift amounted to 20 MHz.

Investigation of the antenna characteristics of the heterodyne detector were carried out with Ge-Au and Ge-Zn-Sb photoresistors. Both photoresistors have a 2×2 mm detection area, and they were cooled to a temperature of 78%K.

The scanning mirror was set to within ±0.05 mm.

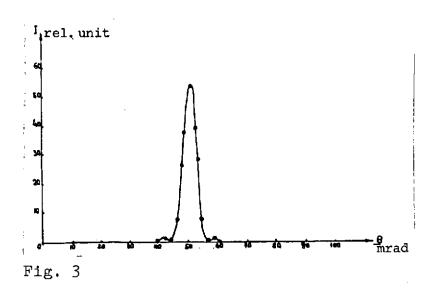


The results of measurements of the directivity characteristics of the heterodyne detector of the $\rm CO_2$ laser emitter are presented in Fig. 2. The nature of the curve obtained coincides quite well with that calculated theoretically. According to the estimate of the detection area size, for which coherent detection conditions were satisfied in our experiment, is 0.15×0.15 mm.

To compare the directivity patterns of the direct and heterodyne detection, it is sufficient to overlap the heterodyne beam The results of the comparison are presented in Fig. 2. The gain of the output signal, using heterodyne detection, is 20 dB, and the directivity pattern is narrowed 15-fold, to 0.007 rad.

In determination of the detector directivity, the superhigh frequency reciprocity theorem can be used, which, applied to our case, is formulated in the following manner: "If a photodetector is replaced by a mirror having the same configuration as the detection area of the photodetector and, if the reflected heterodyne beam passes through all those elements, through which the incident signal beam must pass in the forward direction, the distribution of the heterodyne field obtained in a distant zone gives the heterodyne detector directivity pattern."

/44



Using a goldplated metallic mirror,

2 × 2 mm in size, we
obtained the directivity
pattern represented in
Fig. 3. Visualization
and measurement of the
heterodyne field distribution was accomplished by the
thermographic method.

A comparison of the curves of Figs. 2

and 3 shows that the generalized reciprocity theorem can be used to estimate the directivity of a heterodyne detector.

Atmospheric turbulence may cause fluctuations in the arrival angle of the signal. In this case, the heterodyne detection directivity may prevent detection of a weak signal. Use of a

point diode or isotropically radiating heterodyne as a nonlinear element eliminates this effect.

The authors are grateful to A.M. Prokhorov for his attention to the work and for stimulating discussions.

REFERENCES

- 1. Siegman, A.E., Harris, S.E. and McMurty, B.J., Optical Masers, N.Y., Polytechnic Press, 1963, p. 511.
- 2. Teich, M.C., PIEE 56, 37 (1968).
- 3. Karlov, N.V. and Prokhorov, A.M., RIE $\underline{2}$, 2088 (1964).
- 4. Miller, S.E. and Tillotson, L.C., PIEE 54, 1310 (1966).
- 5. Siegman, A.E., PIEE 54, 1350 (1966).